Drop Test Analysis of a LAMY Pencil

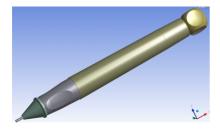
Dr.-Ing. Matthias Hörmann, Steffen Schiele, CADFEM GmbH Reinhard Probol, LAMY GmbH

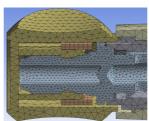
Summary:

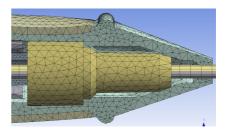
Consumer products like cell phones, personal digital assistants, dish washers or cookers, to name just a view of them, are often exposed to drop during transportation to the customer and during usage in life time. Pre-damage, failure or malfunction due to drop is typically not acceptable and will lead to refusal through the costumer in addition with a correspondingly amount of financial and prestige loss.

The present work deals with the numerical simulation of a drop test of a LAMY pencil. Special emphasis is put on the drop onto the apex of the pencil, which is most harmful to the lead mechanics. In experiments, failure of the lead mechanics was observed for this drop position, which was a result of localized high stresses in combination with plastification in those regions.

It was the goal of the simulations to investigate whether an exchange of the used material for the lead mechanics would meet the requirements. Special emphasis was hereby placed on the reproduction of the overall lead kinematics translational and rotational wise as well as to account for the behavior of the floor material.







Keywords:Droptest, Material failure, Consumer products



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LAMY & CADFEM



ANSYS Competence Center FEM



Motivation

Motivation for this Pencil

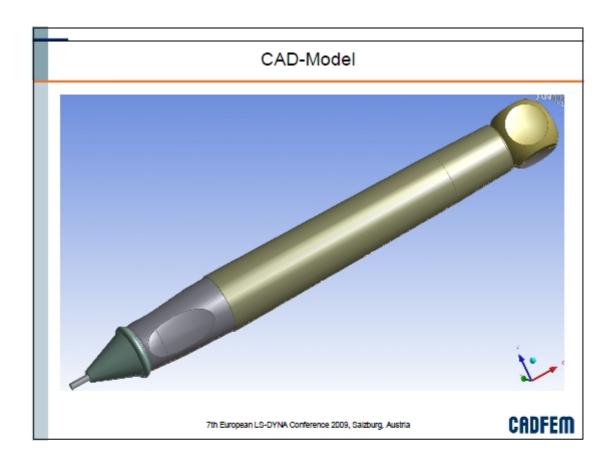
- Failure in the lead mechanics during drop test observed using Ultraform material
- Investigation of other material combinations in order to fullfil drop test requirements
- > No change in production tools allowed because of cost requirements

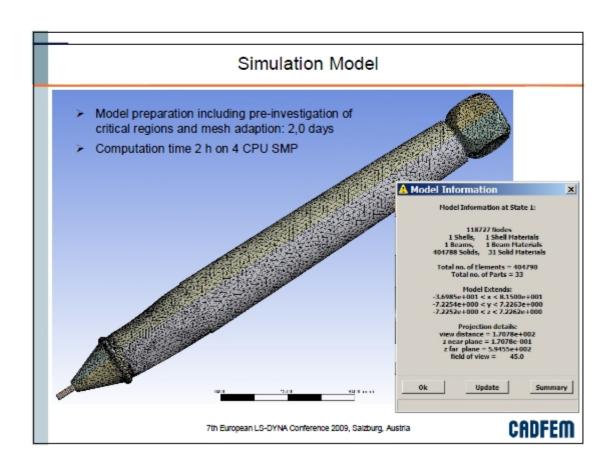
Long-term Motivation

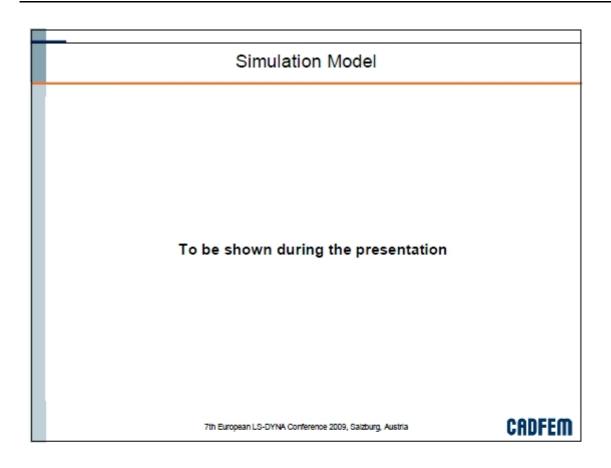
- ➤ Simulation of all relevant loading cases (drop test, bending, clip loading, etc.) upfront in order to detect weaknesses in design at much earlier development state → Upfront Simulation
- ➤ Reduce development cycle time and costs due to less experiments and prototypes
 → Reduce Time to Market
- ➤ Get detailed insight into the pencil for all structural parts (glassy pencil) in order to get thorough understanding of behavior and derive/detect potential for optimization → Saving Material and Costs

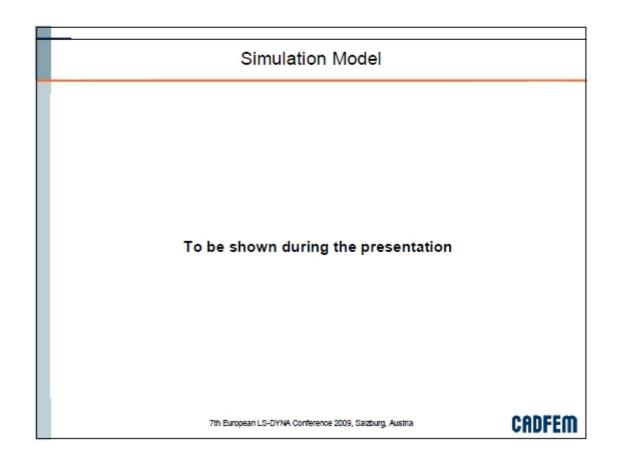
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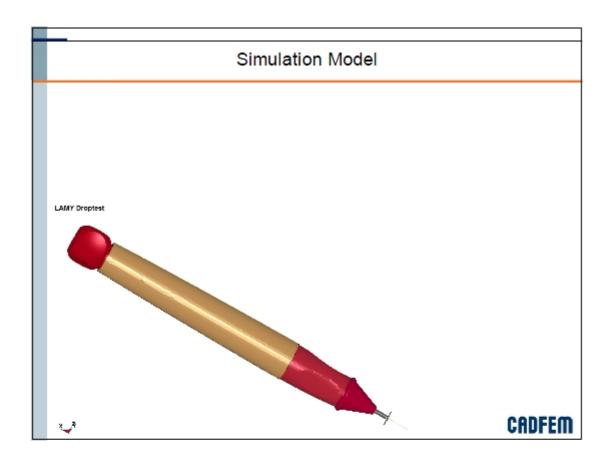
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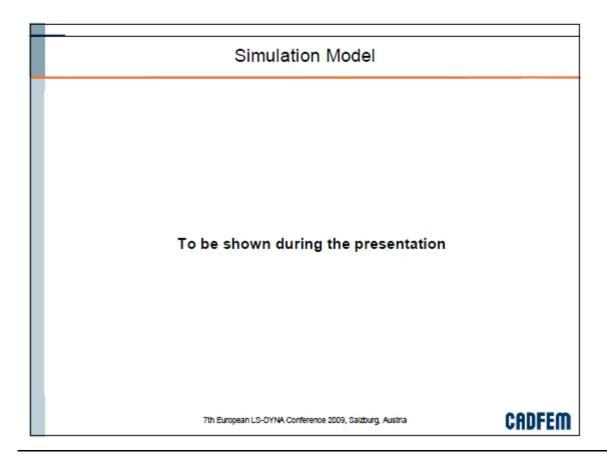












| Materials | | | | | |
|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------|-----------------------------------------------------------------------------|--|--|
| Material Properties Ultra | form S2 | 320, | BASF | | |
| Produktmerkmale | | | | | |
| Polymer-Kunzesit/ten Dichte Wassersufnahme, Sattigung in Wasser bei 23°C Feuchtigkeiberuhsehme, Sättigung bei Normalkling 23°C/S0%r F | ISO 1183 ahrlich ISO 62 ährlich ISO 62 | kg/m² % % | 1400 0.8 0.2 | | |
| Verarbeitung | | | | | |
| Verarbeitungsverfahren: Spritzgießen (M), Extrusion (E), Blastormen (E) Schmetztemperatur, USC Schmetze Volumenrate MVR bei 180 °C und 2,16 kg Massetemperaturbereich, Spritzgießen Werkzeugtemperaturbereich | ISO 11357-17-3 ISO 1133 | cmV10min | M 167 11 190 - 230 60 - 100 | | |
| Werkstoffkennwerte zum Brennverhalten | | | | | |
| Pristong nach Ull-Standard bei d = 1,8 mm Dicke K/z-Innenausstattung: Dicke ≥= 1mm | UI -94 - | dass. | нв + | | |
| Mechanische Eigenschaften | | | | | |
| Zug-E-Mockil Streckteparnung, 50 mm/min Streckteparnung, 50 mm/min Nommelle Bruchdehnung, 50 mm/min Zug Kireshmodul, 1000 in, Dehnung x= 0,5%, 23°C Charpy-Schlagzshigkeit (23°C) Charpy-Schlagzshigkeit (30°C) Charpy-Kerbachtegzshigkeit (30°C) Charpy-Kerbachtegzshigkeit (30°C) Charpy-Kerbachtegzshigkeit (30°C) Kugeldnockharte H Prüfereit Zahtdauer | ISO 527-11-2 ISO 527-11-2 ISO 527-11-2 ISO 527-11-2 ISO 599-1 ISO 179/1eU ISO 179/1eU ISO 179/1eA ISO 2339-1 ISO 2339-1 ISO 2339-1 | MPa MPa % MPa MPa kJ/m² kJ/m² kJ/m² kJ/m² kJ/m² | 2700 65 9 28 1300 180 170 5.5 5 145 358 30 | | |

Materials

Material Properties Delrin, DU PONT

| Property | Test Method | Units | Value |
|-----------------------------|--------------|-------|--------|
| Mechanical | | | _ |
| Yield Stress | 180 527-17-2 | MPn | (72) |
| Yield Strain | 180 527-17-2 | 55 | 13 |
| Nominal Strain at Break | ISO 527-1/-2 | 80 | 30 |
| Strain at Break | ISO 527-1/-2 | 95 | (45) |
| Fensile Modulus | ISO 527 1/2 | MPz. | 3200 |
| Fensile Creep Modulus | 180 899 | MPa | |
| 1h | 1 | | 2900 |
| 1000h | | | 1700 |
| Flexural Modulus | ISO 176 | MPa | 3000 |
| Notched Izod Impact | ISO 180/1A | k3/m2 | |
| -40C | | 1 7 1 | 9 |
| 23C | | | 9 |
| Notched Charpy Impact | ISO 179/1cA | k3/m2 | |
| 30C | | | 8 |
| 23C | | | 9 |
| linustriusi Charpy Impact | ISO 179/1eU | k.bm2 | |
| -300 | | * *** | 100 |
| 23C | | | 340 |
| hermal | | | |
| Deflection Temperature | ISO 75-1/-2 | 'C | |
| 0.45MPa | | | 1.65 |
| 1.80MPa | 1 1 | | 100 |
| 1.80MPa, Annealed | 1 1 | | 115 |
| Melting Temperature | ISO 3146C | °C | 178 |
| Viest Softening Temperature | ISO 306 | °C | |
| 50N | | | 160 |

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Materials

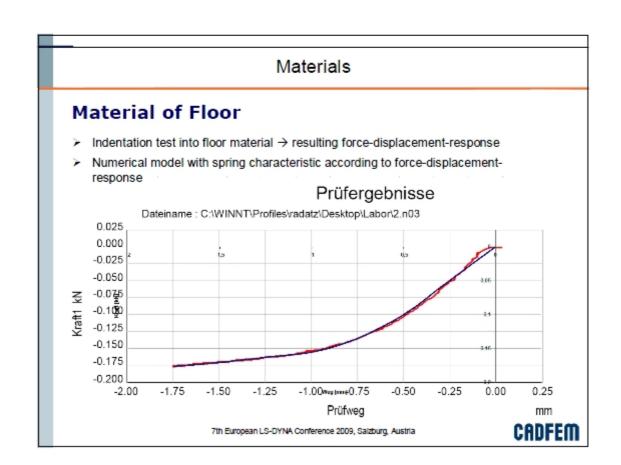
Comparison of Ultraform and Delrin

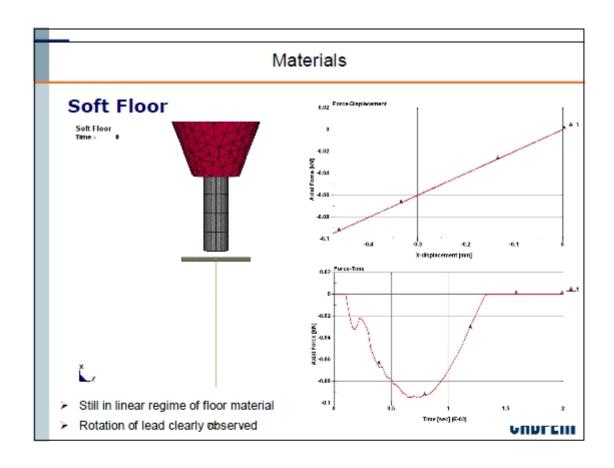
| | Ultraform | Delrin |
|--------------------------|-----------|--------|
| Density [kg/m3] | 1400 | 1420 |
| Young's Modulus [MPa] | 2700 | 3200 |
| Yield Strength [MPa] | 65 | 72 |
| Strain at Break [%] | 28/ | 30/45 |

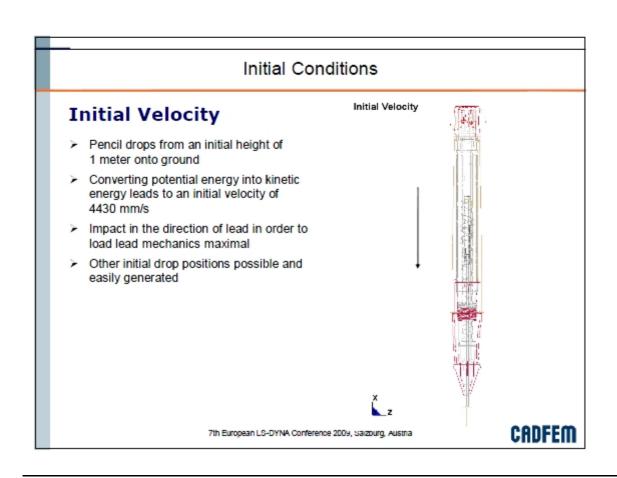
- No nonlinear stress-strain characteristic available
 - → simplified approach with bilinear stress strain curve
- ➤ No information on strain rate dependency of material → not accounted for

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Ultraform Deformation To be shown during the presentation Extensive bending of lead observed → material properties & failure? Rotation of lead according to winding in pencil Localized deformation in lead mechanics 7th European LS-DYNA Conference 2009, Salzburg, Austria

Ultraform Deformation & von Mises Stress To be shown during the presentation Extensive bending of lead 7th European LS-DYNA Conference 2009, Salzburg, Austria

Conclusions

General

- ➤ Extensive bending of lead is observed → proper material parameters needed and inclusion of lead failure might be necessary
- Rotation of lead mechanics due to winding slope in pencil is reasonable
 model represents overall kinematics of pencil
- Comparison with high speed movies is necessary

Material Ultraform

- Simulation of drop test using Ultraform simplified material properties shows indication for failure in lead mechanics
- > Localized permanent deformations and high plastic strains can be observed
- Failure and damage on winding slope might be critical and must be checked

Material Delrin

- Simulation of drop test using Delrin simplified material properties shows clear improvement and no indication for failure in lead mechanics
- Less localized permanent deformations and smaller plastic strain can be observed

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