

Improving Crash Analysis Through the Estimation of Residual Strains Brought About by Forming Metal

William Broene, PE
Manager of Engineering Services
Brown Corporation of America
Ionia, Michigan 48846
Email: bbroene@browncorp.com

ABSTRACT

This paper describes a method that can be used to estimate the residual strains from the forming of sheet metal without running forming simulations. For a first-order crash analysis, using estimated residual strains rather than the strains reported from several forming simulations increases the speed of the design process. The method estimates residual forming strains from the part geometry itself and assumes that the part was formed from a planar sheet of metal.

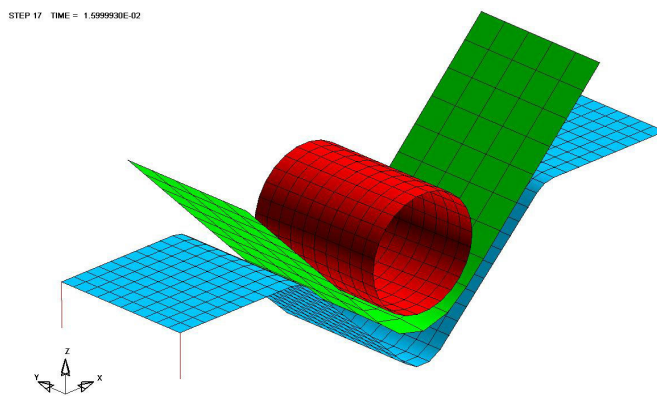
The importance of considering the forming history of a part is demonstrated by comparing crash analysis results with and without the consideration of these residual strains. Along with this, physical test results will be compared of a part as formed and an identical part which was heat treated to relieve some of the cold working strains.

Once the importance of considering forming history has been established, an alternative method of estimating residual strains will be examined. Crash analysis results using forming simulation residual stresses and strains will be compared to analysis results using estimated strains from the alternative method.

Finally the scope of application of this strain estimation method will be discussed.

1 Importance of Including Forming Strains

An LS-DYNA model was created to analyze the forming process of a simple part. The guidelines in the paper: [Input Parameters for Metal Forming Simulation using LS-DYNA](#), by Bradley N. Maker were followed in creating the model and the LS-DYNA input deck is included in the appendix.

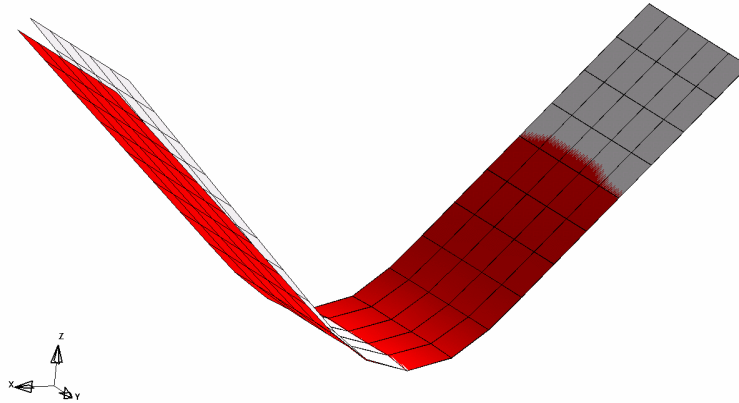


Forming Simulation

The *INTERFACE_SPRINGBACK keyword was used so that the residual stresses and strains from the analysis would be written to a *dynain* file. This same *dynain* file is included in an LS-DYNA implicit run that models the spring back.

The spring back model was developed using the guidelines from: [Input Parameters for Springback Simulation using LS-DYNA](#) also by Bradley N. Maker. This model is included in the appendix. Once again, the *INTERFACE_SPRINGBACK keyword was used so the residual stresses and strains could be used in the crash simulation.

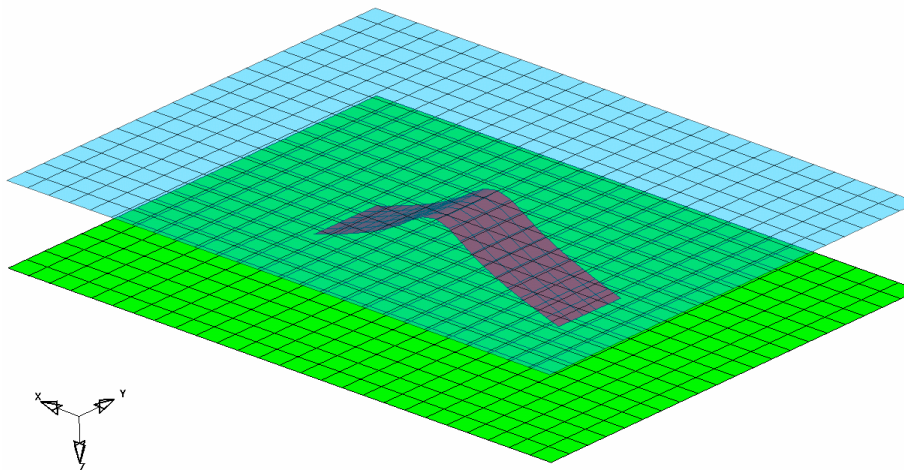
STEP 6 TIME = 2.000000E-02



Spring Back Simulation

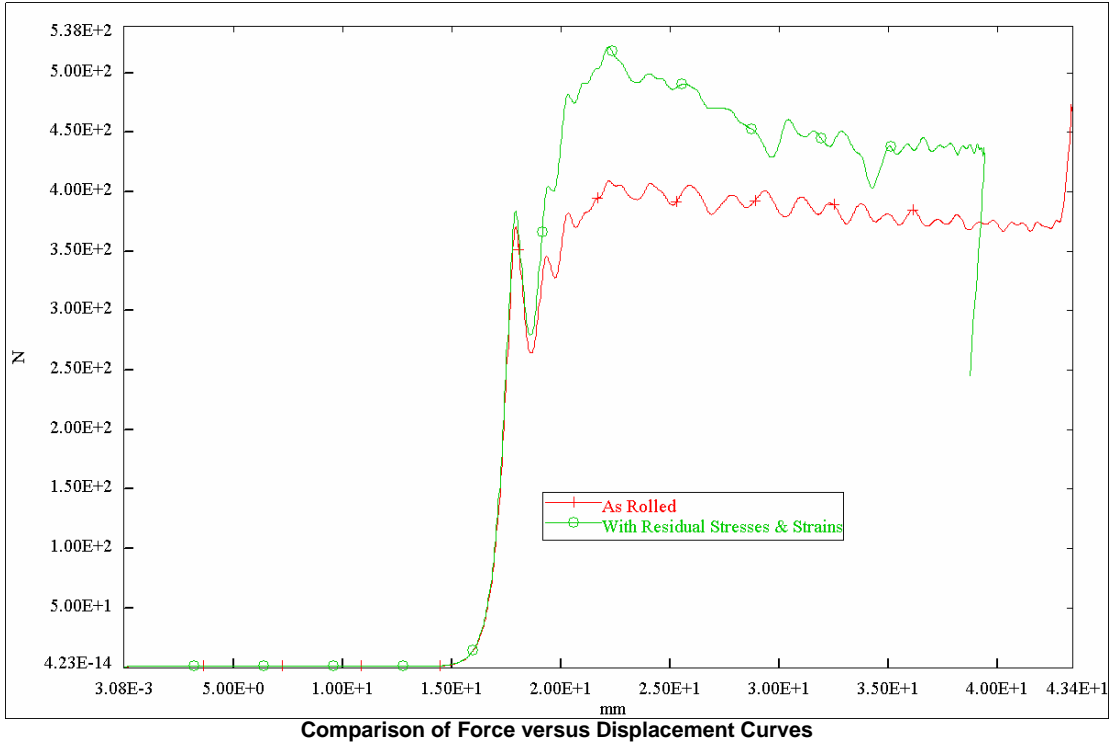
Two LS-DYNA crash models were developed. One model used the *INITIAL_STRESS_SHELL cards from the *dynain* file obtained from the spring back analysis while the other model did not use them. Running these two models allow the comparison of crash analysis results with and without the consideration of cold work from the forming process. The LS-DYNA input deck for this is included in the appendix.

STEP 10 TIME = 4.4995341E-03



Crash Simulation

The Graph below represents the force versus displacement relationship from both of the crash simulations.



The table below lists the percentages of error that result when the forming stresses and strains are ignored. The crash analysis using residual stresses and strains is assumed to be ideal.

Model	1st Peak Load	Error	Displacement	Error
As Rolled	410 N	-21%	43.4 mm	+11%
With Stresses and Strains	522 N	0	39.2 mm	0

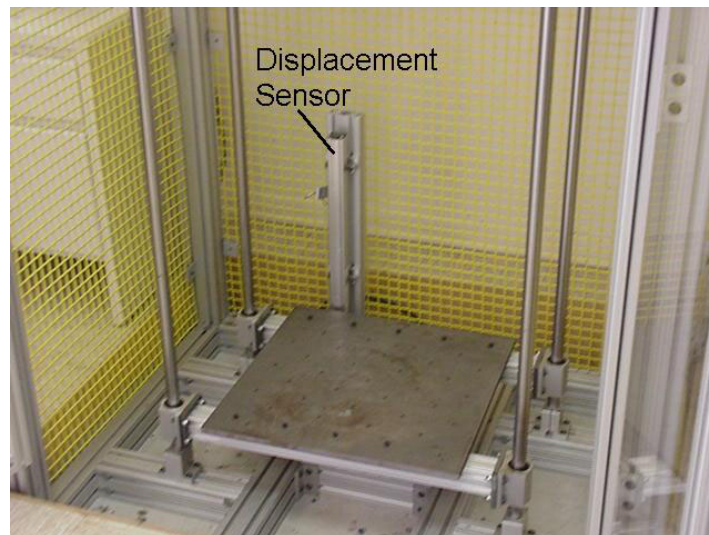
Error Analysis Table

Physical Test

A physical drop tower test was run on two identical parts. One part was heat treated for 8 hours at 800° F then air-cooled to relieve some of the strains from forming while the other was crushed without any treatment after forming.



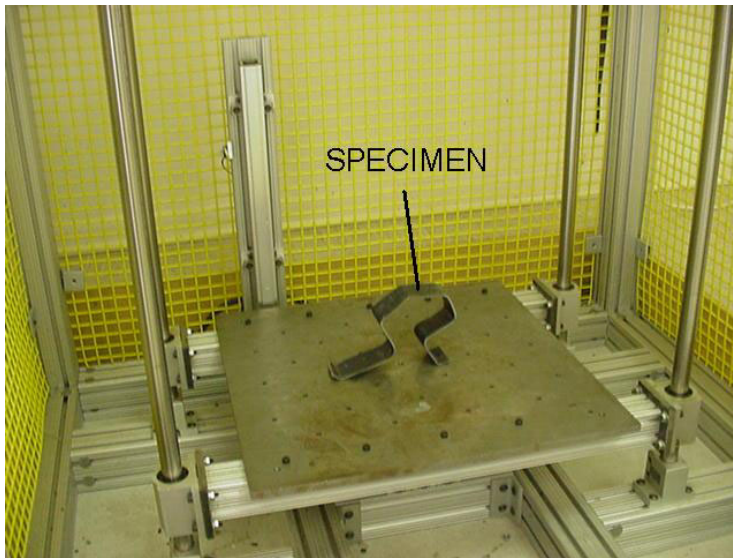
Drop Tower Test Machine



Displacement Sensor in Drop Tower



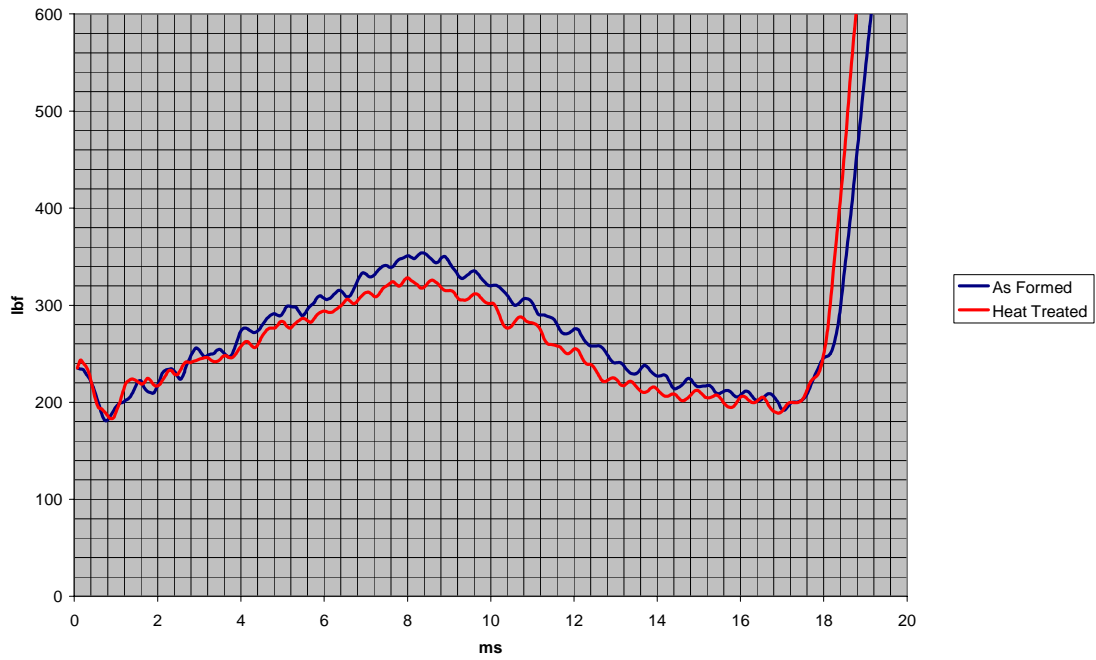
Load Sensor in Drop Tower



Placement of Specimen on Mounting Plate

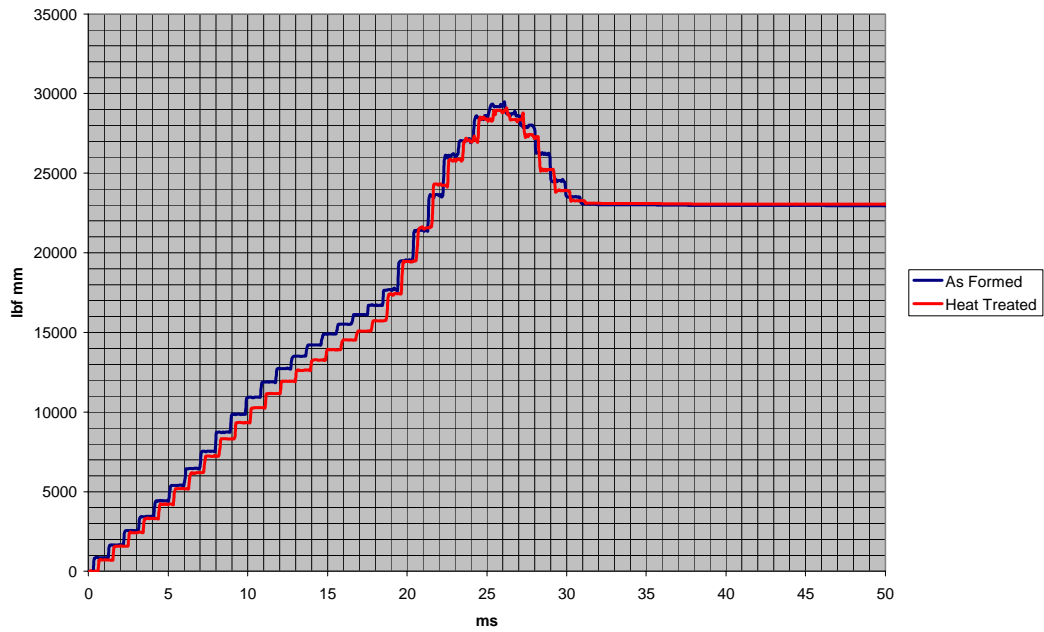
The parts tested had just one 90° bend. The results are as follows.

Loads

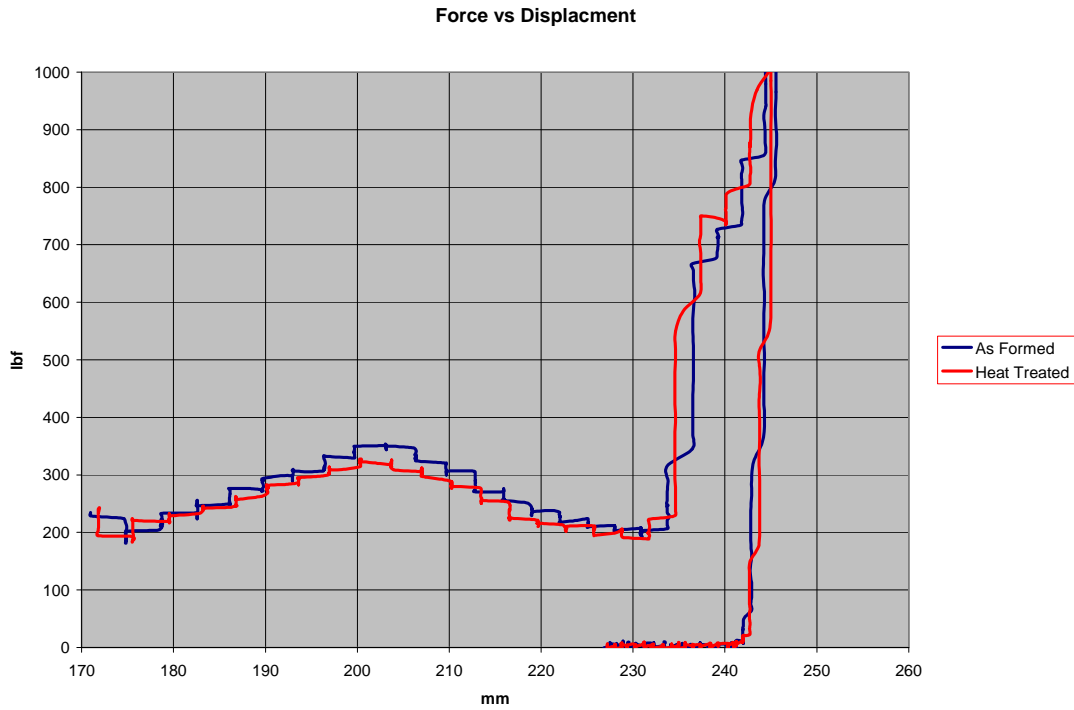


Crushing Force vs. Time

Energies



Energy Absorbed vs. Time



Crushing Force vs. Displacement

The table below lists the percentages of discrepancy between the heat treated and non-heat treated parts when crushed in the drop tower.

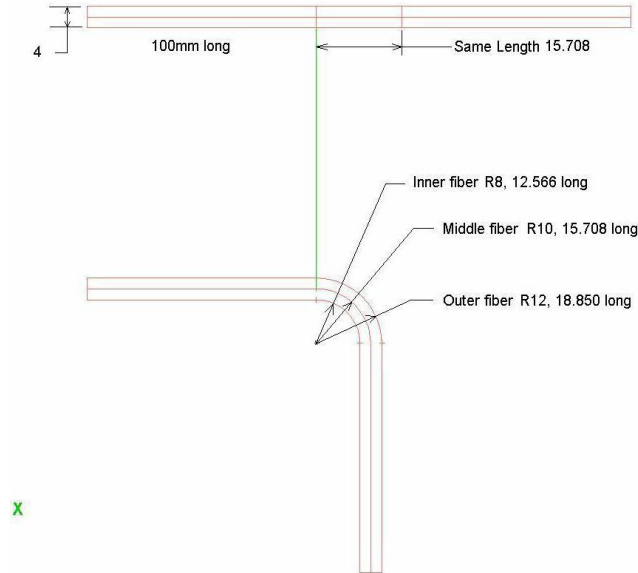
Model	1st Peak Load	Delta	Displacement at 1st Peak Load	Delta
As Formed	350 lbf	0	203.13 mm	0
Heat Treated	318 lbf	-9 %	203.73 mm	+0.3%

Error Analysis Table

Whether or not all of the cold work from forming was removed from the heat treated part is unknown. The purpose of the physical test is to show that there is a difference in crushing performance based on the amount of cold work or residual strains in a formed part.

2 Theory behind Strain Estimation

The illustration below illustrates the change in length of the inner and outer fibers after bending 90°.



Approximate Fiber Lengths after Bending 90°

The average plastic strain in the bend area for each fiber is the change in fiber length divided by the original length. All fibers are 15.708 mm long before bending over an 8mm radius die. After bending, the fiber lengths become:

$$l_f = r_f \theta$$

where θ is the bend angle in radians.

r is the radius of the fiber

Average plastic strains along each fiber are estimated by:

$$\epsilon_f = \frac{r_f \theta - l_m}{l_m}$$

where l_m is the approximate length of the middle fiber. Putting this all in terms of radii and angles gives:

$$\epsilon_f = \frac{r_f \theta - r_m \theta}{r_m \theta}$$

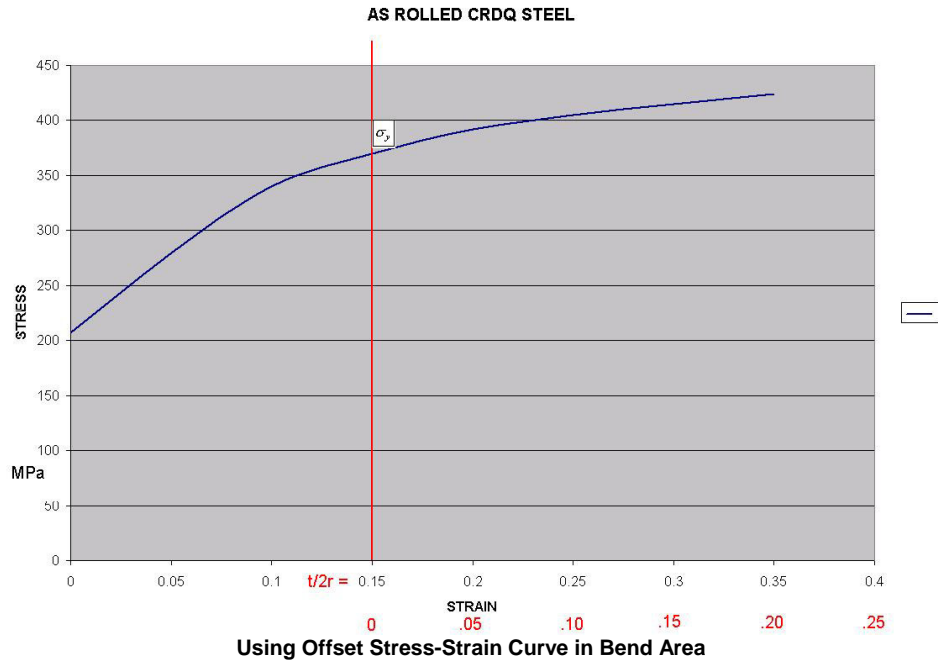
Canceling out the angle and expressing in terms of the middle radius and metal thickness gives an expression for the average plastic strain in the bend area of the outer and inner fibers.

$$\epsilon = \pm \frac{t}{2r_m}$$

where t is the thickness of the formed part and r_m is the mid-surface radius of the part.

3 Manual Application of Method

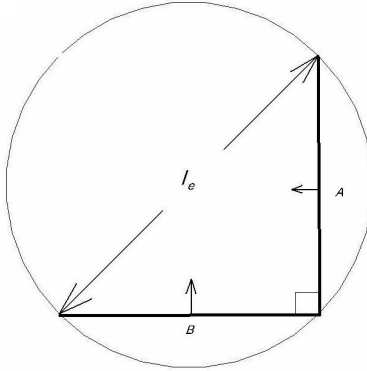
Although tedious, material properties could be modified in the bend area of parts by offsetting the stress-strain curve by the estimated plastic strain. The new yield strength would become the as-rolled stress level when the as-rolled strain is equal to $t/2r - .002$. The new stress value when the new strain is at .05, for example, would be the same as when the as rolled strain is at $t/2r + .048$.



It may be a good idea to use a de-rating factor on $t/2r$ since that absolute value of strain occurs at the outer and inner-most fibers.

4 Automation of the Method

An algorithm has been developed and implemented in a computer program for the processing of LS-Dyna input files to obtain estimated residual plastic strains from the forming process. To adapt the formula $t/2r$ to shell elements, a formula in terms of the angle between two neighboring elements and their length was needed. The following observation was made.



Let ϕ be the angle between segments A and B.

Note that:

$$\frac{\sin \phi}{l_e} = \frac{1}{2r}$$

And:

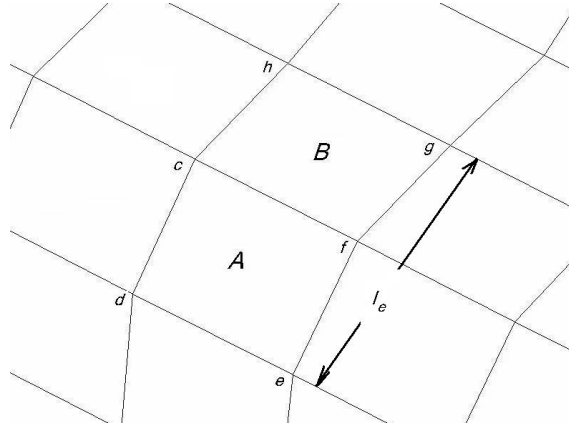
$$\frac{t \sin \phi}{l_e} = \frac{t}{2r} = |\epsilon_p|$$

From this observation, the following conclusions are made.

The average plastic strain from forming in a given element can be estimated by:

- (1) The angle between its normal vector and those of its neighboring elements [ϕ]
- (2) The thickness of the element. [t]
- (3) The length of the element and the length of its neighboring elements. [l_e]

Algorithm



1 Parse the LS-Dyna input file.

2 For each element, (element A) do:

2.1 Determine thickness (get PID to find SID)

2.2 For each element edge do:

2.2.1 Find a neighboring edge if it exists

2.2.2 Estimate plastic strain, \mathcal{E}_p

2.2.2.1 Calculate normal vector of element A.

$$\vec{fc} \times \vec{cd} = \vec{N}_A$$

2.2.2.2 Calculate normal vector of element B

$$\vec{cf} \times \vec{fg} = \vec{N}_B$$

2.2.2.3 Calculate the angle between normals

$$\phi = \cos^{-1} \left(\frac{\vec{N}_A \cdot \vec{N}_B}{|\vec{N}_A| |\vec{N}_B|} \right)$$

2.2.2.4 Calculate distance of farthest edges, l_e

Average the distances of each pair of nodes belonging to separate elements.

$$l_e = \frac{|\vec{dh}| + |\vec{dg}| + |\vec{eh}| + |\vec{eg}|}{n}$$

where: $n=4$ for (2) quadrilateral elements
 $n=2$ for (1) quad and (1) tria element
 $n=1$ for (2) triangular elements

2.2.2.5 Calculate plastic strain relating elements A and B. (B is current neighbor being evaluated)

$$\mathcal{E}_p = \frac{t \sin \phi}{l_e}$$

2.2.2.6 Store \mathcal{E}_p for comparison to values from other neighboring elements.

2.2.3 Next edge

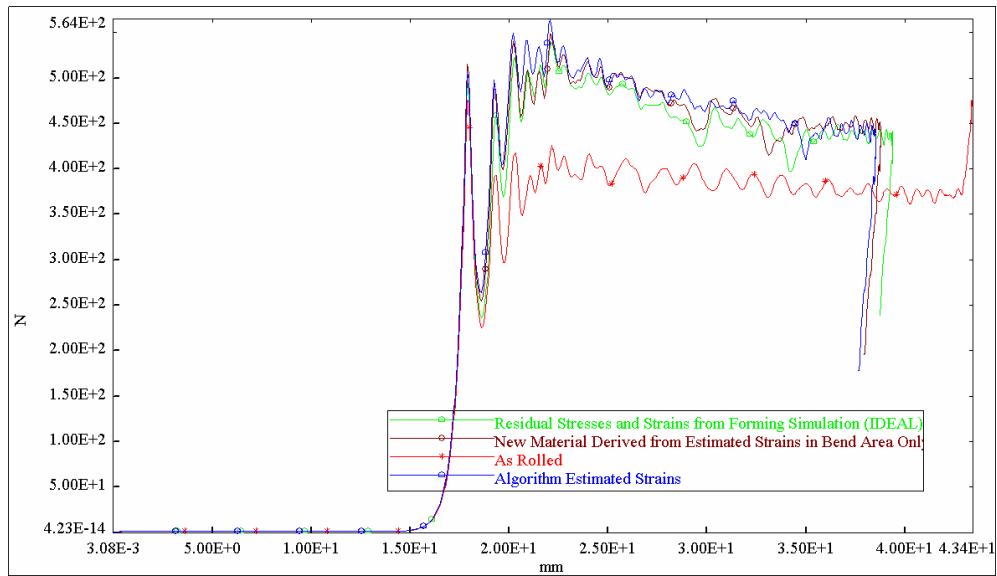
2.3 Store highest \mathcal{E}_p found for element A.

2.4 Write out *INITIAL_STRESS_SHELL cards.

```
*INITIAL_STRESS_SHELL
$-----1-----2-----3-----4-----5-----6-----7-----8
$      EID      NPLANE      NTHICK
      A          40          5
      0          0          0          0          0          0          0          0
-9.062E-1      0          0          0          0          0          0          0          ep
-5.385e-1      0          0          0          0          0          0          0          .59ep
 5.385e-1      0          0          0          0          0          0          0          .59ep
 9.062E-1      0          0          0          0          0          0          0          ep
```

2.5 Next element

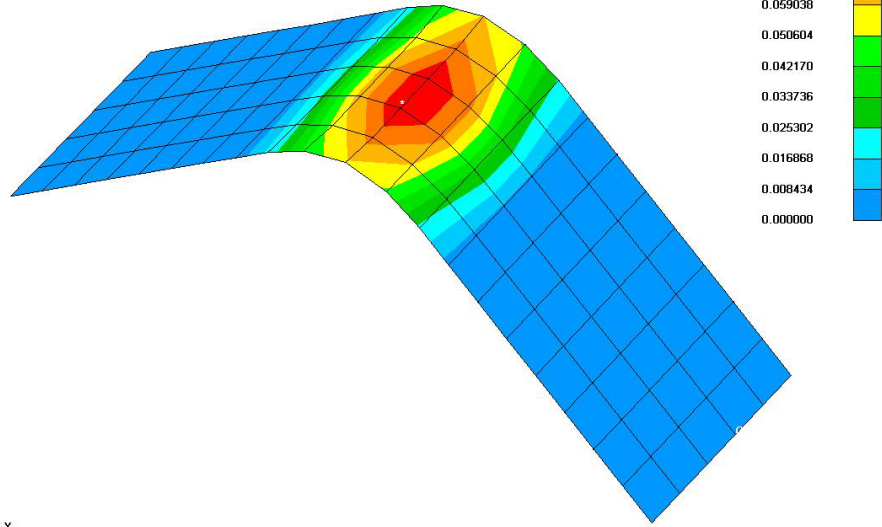
3 Comparison of Results Using Different Methods



Study 1 [SIMPLE BEND]: Comparison of Force vs. Displacement Curves

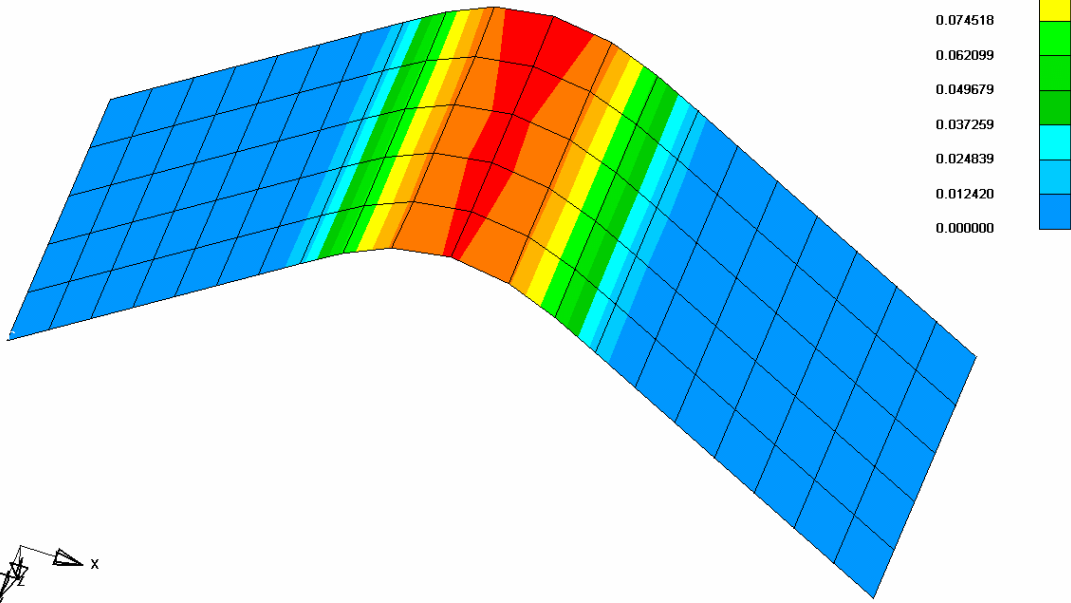
The graph above shows force versus displacement curves for four different LS-DYNA crash simulations. The lowest curve was obtained from the simulation using as-rolled steel properties. The manual strain estimation method and the automated method results are relatively close to the results of the simulation that used stresses and strains from the forming simulation. For this simple case, it is evident that considering forming effects (even estimated), will improve performance accuracy.

CRASH MODEL,
STEP 2 TIME = 4.9978605E-04
EF PLASTIC STN(T)



[FORMING] Effective Plastic Strains at Top Fiber

CRASH MODEL, AS ROLLED
STEP 2 TIME = 4.9978984E-04
EF PLASTIC STN(T)

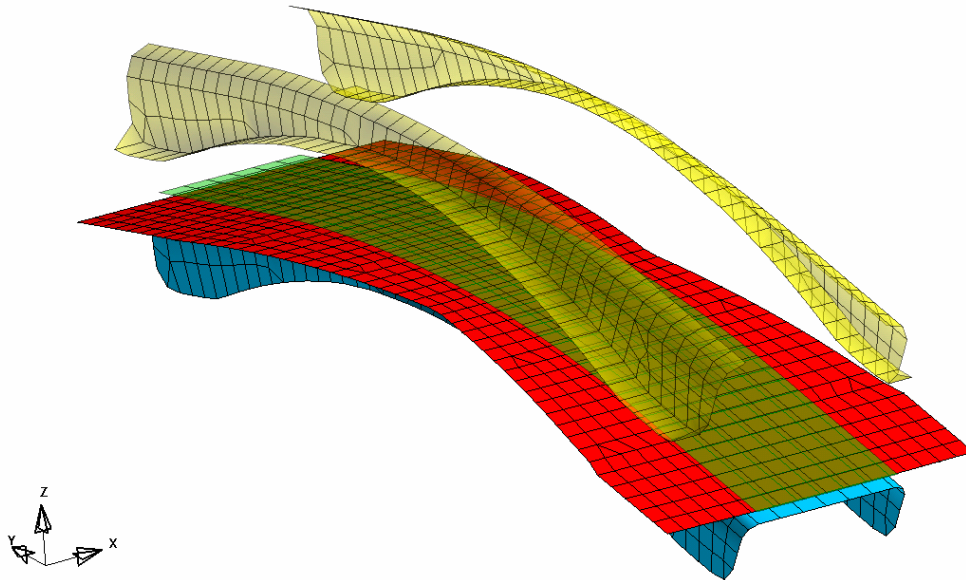


[ESTIMATED] Effective Plastic Strains at Top Fiber

Study of Drawn Bracket

FORMING EA

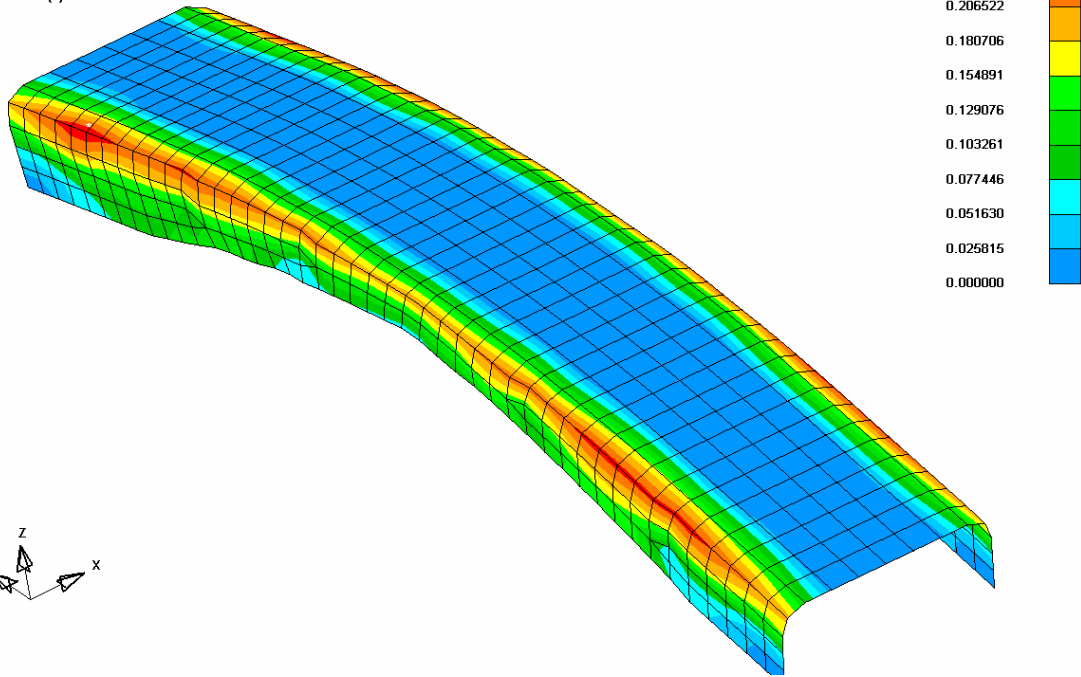
STEP 12 TIME = 2.1999920E-02

**Study 2 Forming Simulation**

The forming simulation for a steel bracket models the forming station of a progressive stamping die. A one half inch strip of steel on each short end of the blank carries the part from one station in the die to the next. To model this strip, X and Y constraints were used on one end of the blank while the other end had X constraints assigned. First a pad comes down to press the blank in a crown shape, then two blocks come down to wipe the flanges.

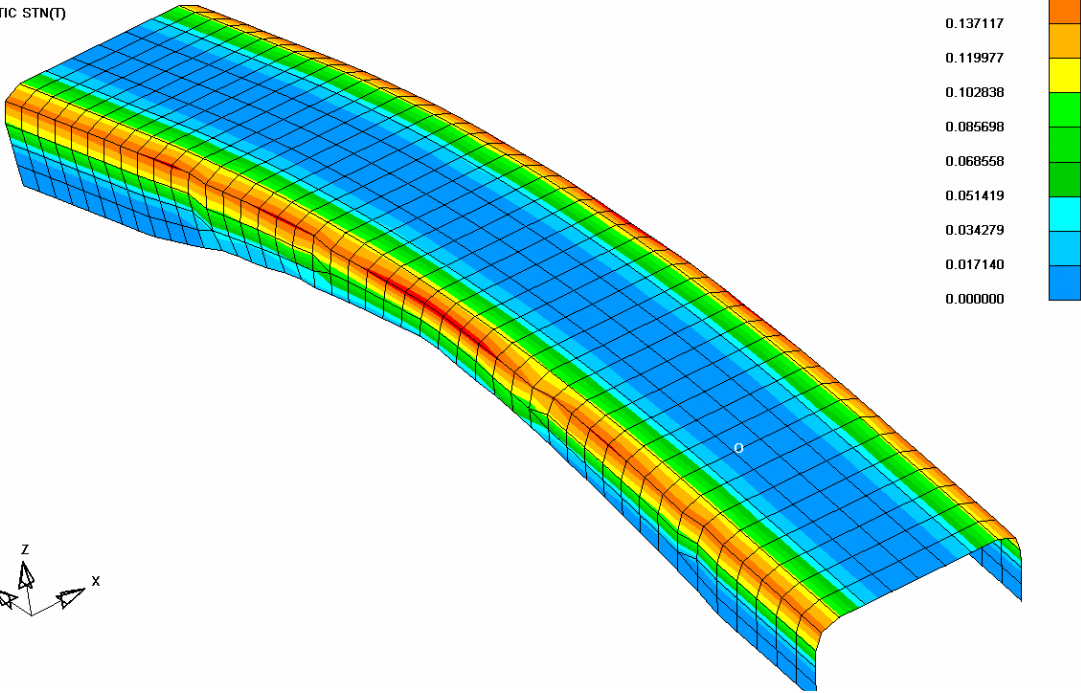
A dynain file is written out to be used as input for the springback simulation. Once the springback simulation has finished, another dynain file is written out so the stresses and strains can be initialized in one of the crash simulations.

EA CRASH AS ROLLED
STEP 2 TIME = 9.9981087E-04
EF PLASTIC STN(T)

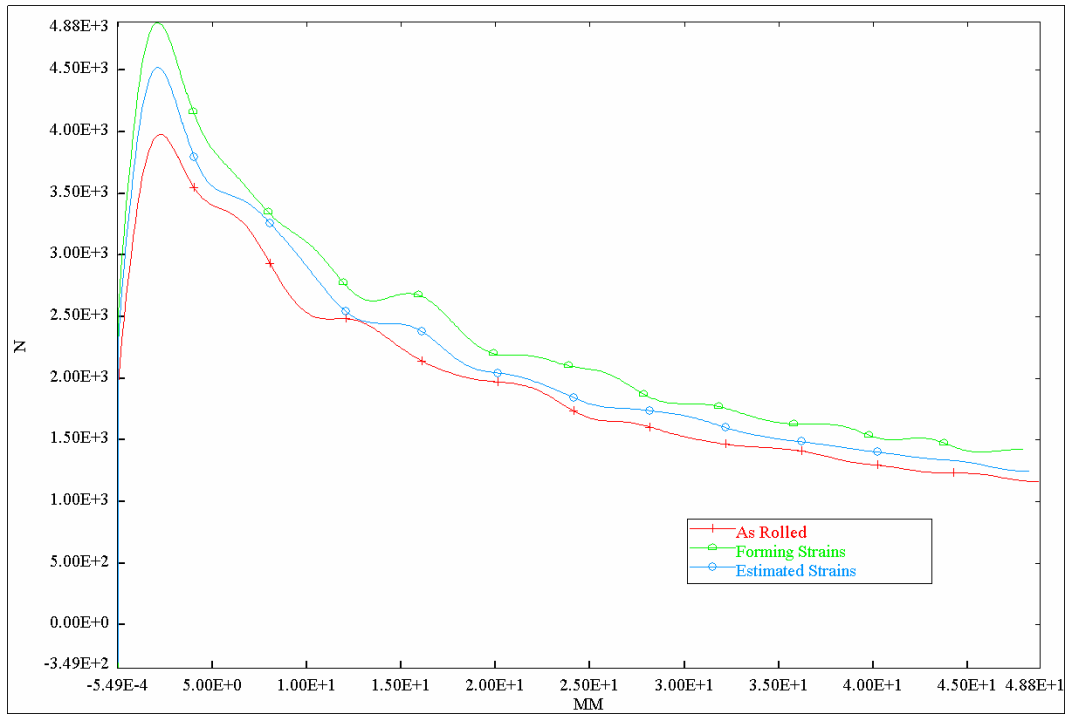


[FORMING] Effective Plastic Strains at Top Fiber

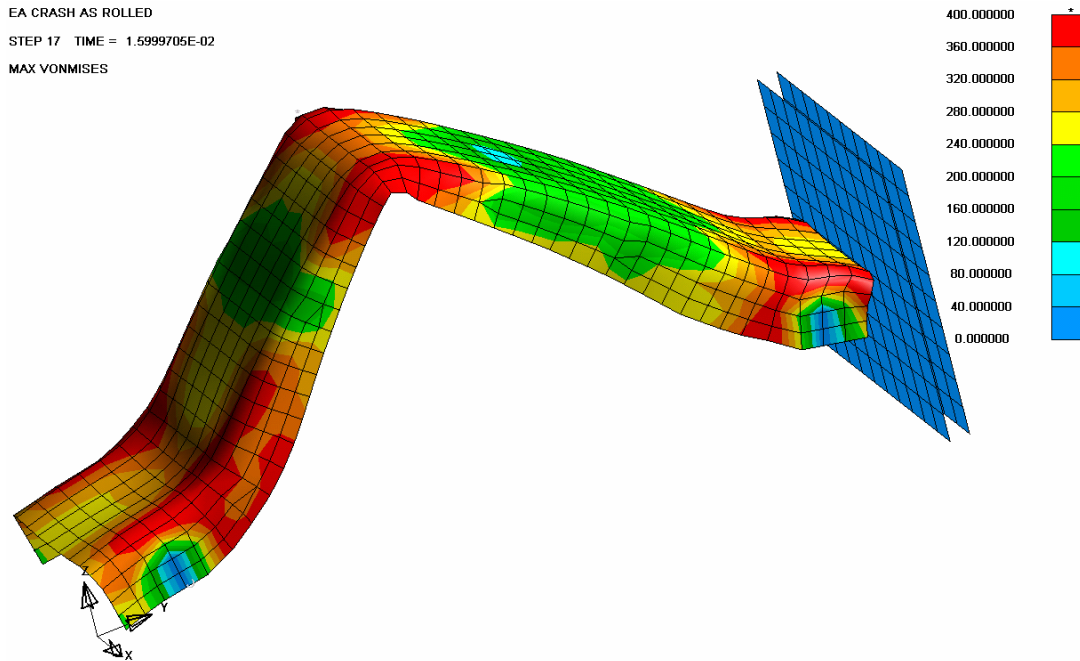
EA CRASH AS ROLLED
STEP 2 TIME = 9.9983369E-04
EF PLASTIC STN(T)



[ESTIMATED] Effective Plastic Strains at Top Fiber



Study 2 [Drawn Part]: Comparison of Force vs. Displacement Curves



Study 2 [Drawn Part]: Crash Model

4 Scope of Method Application

The method applies to formed metal parts where no significant change in material thickness occurs. The residual plastic strains from simple or compound bending are estimated but those resulting from stretching are not. (The strains in stretch formed parts will be underestimated by the method.)

This method should not be used on poor quality meshes.

5 Conclusion

The accuracy of crash analysis on initially-flat metal parts that contain bends and use as-rolled material properties will improve by incorporating the strains that are estimated by this method.

REFERENCES

LSTC (1999), *LS-DYNA User's Manual Version 950*, Livermore Software Technology Corporation.

Cowell, B., *The Effects of Forming and Parameter Mapping on Further Simulation*, 6th annual LS-Dyna User's Conference, 2000

Maker, B., and Zhu, X., *Input Parameters for Springback Simulation using LS-DYNA*, 2001

Maker, B., and Zhu, X., *Input Parameters for Metal Forming Simulation using LS-DYNA*, 2000

ACKNOWLEDGEMENTS

This work has been carried out as part of an independent study at Kettering University under the supervision of Raghu Echempati, Ph.D.

APPENDICES

A1 Forming Analysis Input Deck

```

*KEYWORD
$-----1-----2-----3-----4-----5-----6-----7-----8
$
$ DYNAD(936) DECK WAS WRITTEN BY: RTA/PEMB VERSION 26
$ DATE : Jan 24, 2002 at 10:35:52
$
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (1) TITLE CARD.
$-----1-----2-----3-----4-----5-----6-----7-----8
*TITLE
PUNCH RADIUS 8, THICKNESS 2
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (2) CONTROL CARDS.
$-----1-----2-----3-----4-----5-----6-----7-----8
*CONTROL_TERMINATION
$ ENDTMR ENDNCYC DTMIN ENDMAS ENDMAS
0.020E+00 0 .000 .000 100
*CONTROL_TIMESTEP
$ DTINIT SCFT ISDO TSLMT DTMS LCTM ERODE MSIST
.000 .900 0
*CONTROL_HOURLASS
$ IHQ OH
4 .100
*CONTROL_BULK_VISCOSITY
$ Q2 Q1
1.500 .060
*CONTROL_SHELL
$ WRPANG ITRIST IRNXX ISTUPD THEORY BWC MITER
20.000 2 -1 1 2 2 1
*CONTROL_CONTACT
$ SLSFAC RWPNAL ISLCHK SHLTHK PENOPT THKCHG ORLEN
.010
$ USRSTR USRFAC NSBCS INTERM XPENE 0 4.000
*CONTROL_ENERGY
$ HGEN RMEN SLANTEN RYLEN
1 2 1 1
*CONTROL_DAMPING
$ NRCYCK DRTOL DRFCR DRTERM TSSPR IRELAL EDTTL IDRFLG
250 .001 .995
*CONTROL_OUTPUT
$ NFOPT NEECHO NREFUP IACCOF OPIFS IPNINT IKEDIT
0 0 0 0 .000 0 100
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (3) DATABASE CONTROL CARDS - ASCII HISTORY FILE
$-----1-----2-----3-----4-----5-----6-----7-----8
*DATABASE_HISTORY_NODE
$ ID1 ID2 ID3 ID4 ID5 ID6 ID7 ID8
1219 856
*DATABASE_HISTORY_SHELL_SET
$ ID1 ID2 ID3 ID4 ID5 ID6 ID7 ID8
12
*SET_SHELL_LIST
$ SID NUM DA1 DA2 DA3 DA4
$ EID8 EID2 EID3 EID4 EID5 EID6 EID7 EID8
7 8 9 10 11 12 13 14
27 28 29 30 31 32 33 34
47 48 49 50 51 52 53 54
67 68 69 70 71 72 73 74
87 88 89 90 91 92 93 94
$OPTION : BEAM BEAM_SET NODE NODE_SET
$ SHELL SHELL_SET SOLID SOLID_SET
$ TSHLL TSHLL_SET
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (4) DATABASE CONTROL CARDS FOR ASCII FILE
$-----1-----2-----3-----4-----5-----6-----7-----8
$*DATABASE_OPTION
$ DT
$
$OPTION : SECFORC RMPORC NODOUT ELOUT GLSTAT
$ DEFORC MATSUM NCFORC RCFORC DEFQEO
$ SPCFORC SRFORC ABSTAT NODFOR BNDOUT
$ RBDOUT GCBOU SLEOUT MPFS SBTOUT
$ UNIFORM AVSFUT MOVIE
*DATABASE_NODOUT
.400E-04
*DATABASE_ELOUT
.400E-04
*DATABASE_GLSTAT
.400E-04
*DATABASE_DEFORC
.400E-04
*DATABASE_RBDOUT
.400E-04
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (5) DATABASE CONTROL CARDS FOR BINARY FILE
$-----1-----2-----3-----4-----5-----6-----7-----8
*DATABASE_BINARY_D3PLOT
$ DT/CYCL LCDD NOBEAM
.100E-02
*DATABASE_BINARY_D3THDT
$ DT/CYCL LCDD NOBEAM
.100E-02
*DATABASE_BINARY_OPTION
$ DT/CYCL LCDD NOBEAM
$
$OPTION : D3DRFL D3DUMP RUNRSP INTFOR
$-----1-----2-----3-----4-----5-----6-----7-----8
$*DATABASE_EXTENT_BINARY
0 0 3 1 1 1 1 1
0 0 0 0 0 0 0 0
$-----1-----2-----3-----4-----5-----6-----7-----8

```

```

$-----1-----2-----3-----4-----5-----6-----7-----8
$ (6) DEFINE PARTS CARDS
*PART
$-----1-----2-----3-----4-----5-----6-----7-----8
$ PART PID = 1 PART NAME :BLANK
$ PID SID MID EOSID HGID GRAV ADPOPT TMID
$ 1 7 3
*PART
$-----1-----2-----3-----4-----5-----6-----7-----8
$ PART PID = 2 PART NAME :DIR
$ PID SID MID EOSID HGID GRAV ADPOPT TMID
$ 2 8 1
*PART
$-----1-----2-----3-----4-----5-----6-----7-----8
$ PART PID = 4 PART NAME :PUNCH
$ PID SID MID EOSID HGID GRAV ADPOPT TMID
$ 4 6 2
*PART
$-----1-----2-----3-----4-----5-----6-----7-----8
$ PART PID = 5 PART NAME :SPRO001
$ PID SID MID EOSID HGID GRAV ADPOPT TMID
$ 5 5 4
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (7) MATERIAL CARDS
*MAT PIECEWISE LINEAR PLASTICITY
$-----1-----2-----3-----4-----5-----6-----7-----8
$ MATERIAL NAME:HRDQ (Hot Rolled, Draw Quality Steel)
$ RO E FR SICH ETAN EPPF TDEL
$ 3 7.830E-09 2.070E+05 3.000E-01 2.480E+02 0.000E+00 0.000E+00 0.000E+00
$ C P LCSS LCSS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ EBS1 EBS2 EBS3 EBS4 EBS5 EBS6 EBS7 EBS8
$ 0.000E+00 5.000E-02 1.000E-01 1.500E-01 2.000E-01 2.500E-01 3.000E-01 3.500E-01
$ ES1 ES2 ES3 ES4 ES5 ES6 ES7 ES8
$ 2.480E+02 3.260E+02 3.730E+02 4.000E+02 4.150E+02 4.250E+02 4.350E+02 4.500E+02
*MAT RIGID
$-----1-----2-----3-----4-----5-----6-----7-----8
$ MATERIAL NAME:DIE
$ MID RO E PR N COUPLE M ALIAS
$ 1 7.830E-09 2.070E+05 2.800E-01 0.000E+00 0.000E+00 0.000E+00
$ CM1 CM2 CM3 CM4
$ 1.0 4.0 7.0
$ LCO or A1 A2 A3 V1 V2 V3
*MAT RIGID
$-----1-----2-----3-----4-----5-----6-----7-----8
$ MATERIAL NAME:PUNCH
$ MID RO E PR N COUPLE M ALIAS
$ 2 7.830E-09 2.070E+05 2.800E-01 0.000E+00 0.000E+00 0.000E+00
$ CM1 CM2 CM3 CM4
$ 1.0 4.0 7.0
$ LCO or A1 A2 A3 V1 V2 V3
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (7.1) SECTION CARDS
*SECTION SHELL
$-----1-----2-----3-----4-----5-----6-----7-----8
$ PROPERTY NAME:BLANK
$ SID ELFORM SHRP NIP PROPT QR/IRID ICOMP
$ 7 16 .100E+01 5.0 1.0 .0
$ T1 T2 T3 T4 NLOC
$ .200E+01 .200E+01 .200E+01 .200E+01 .0
*SECTION SHELL
$-----1-----2-----3-----4-----5-----6-----7-----8
$ PROPERTY NAME:DIE
$ SID ELFORM SHRP NIP PROPT QR/IRID ICOMP
$ 8 2 .100E+01 2.0 1.0 .0
$ T1 T2 T3 T4 NLOC
$ 2.000E+00 2.000E+00 2.000E+00 2.000E+00
*SECTION SHELL
$-----1-----2-----3-----4-----5-----6-----7-----8
$ PROPERTY NAME:PUNCH
$ SID ELFORM SHRP NIP PROPT QR/IRID ICOMP
$ 6 2 .100E+01 2.0 1.0 .0
$ T1 T2 T3 T4 NLOC
$ 2.000E+00 2.000E+00 2.000E+00 2.000E+00
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (8) NODAL POINT CARDS
*NODE
$-----1-----2-----3-----4-----5-----6-----7-----8
$ NODE X Y Z TC RC
$ 1 .000000000E+00 .200000000E+00 .000000000E+00
$ 2 .399999100E+01 .200000000E+02 .000000000E+00
$ 3 .799999200E+01 .200000000E+02 .000000000E+00
$ 4 .119999300E+02 .200000000E+02 .000000000E+00
$ 5 .159999400E+02 .200000000E+02 .000000000E+00
$ 6 .200000000E+02 .200000000E+02 .000000000E+00
$ 7 .240000000E+02 .200000000E+02 .000000000E+00
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (9) SOLID ELEMENT CARDS
*ELEMENT SOLID
$-----1-----2-----3-----4-----5-----6-----7-----8
$ EID PID N1 N2 N3 N4 N5 N6 N7 N8
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (10) BEAM ELEMENT CARDS
*ELEMENT BEAM
$-----1-----2-----3-----4-----5-----6-----7-----8
$ EID PID N1 N2 N3
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (11) SHELL ELEMENT CARDS
*ELEMENT SHELL
$-----1-----2-----3-----4-----5-----6-----7-----8
$ EID PID N1 N2 N3 N4
$ 1 1 1 22 23 2
$ 2 1 2 23 24 3
$ 3 1 3 24 25 4
$ 4 1 4 25 26 5
$ 5 1 5 26 27 6
$ 6 1 6 27 28 7
$ 7 1 7 28 29 8
$ 8 1 8 29 30 9
$ 9 1 9 30 31 10
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (12) SPRING OR DAMPER ELEMENT CARDS
*ELEMENT DISCRETE
$-----1-----2-----3-----4-----5-----6-----7-----8
$ EID PID N1 N2 VID S PF
$ 1299 5 1468 127 0 .1000000E+01 0 .0000000E+00
$ 1300 5 1470 556 0 .1000000E+01 0 .0000000E+00
$ 1301 5 1471 573 0 .1000000E+01 0 .0000000E+00
$ 1302 5 1469 137 0 .1000000E+01 0 .0000000E+00
*ELEMENT MASS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ EID NID MASS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (14) HOURGLASS AND BULK PROPERTIES CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ HOURGLASS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ IHQ QH IBQ Q1 Q2
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (15) DEFINE SET CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (16) BOUNDARY CONDITION CARDS
*BOUNDARY SPC_NODE
$-----1-----2-----3-----4-----5-----6-----7-----8
$ NID/NSID CID DOFX DOFY DOFZ DOFRX DOFRY DOFRZ
$ 1468 0 1 1 1 1 1 1 1
$ 1469 0 1 1 1 1 1 1 1
$ 1470 0 1 1 1 1 1 1 1
$ 1471 0 1 1 1 1 1 1 1
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (17) LOCAL COORDINATE SYSTEM
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (18) NODAL CONSTRAINT CARDS

```

```

$-----1-----2-----3-----4-----5-----6-----7-----8
$ (22) DEFINE CONTACT SURFACE
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (23) DEFINE RIGID WALL
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (24) NODAL RIGID BODY CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (25) JOINT CARDS
*SECTION DISCRETE
$-----1-----2-----3-----4-----5-----6-----7-----8
$ SID DRO KD VO CL FD
$ 5 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00
$ CDL TDL
$ 0.000E+00 0.000E+00
*MAT SPRING ELASTIC
$-----1-----2-----3-----4-----5-----6-----7-----8
$ MID K
$ 4 3.000E+02
$-----1-----2-----3-----4-----5-----6-----7-----8
*CONTACT AUTOMATIC SURFACE TO SURFACE
$-----1-----2-----3-----4-----5-----6-----7-----8
$ 1 3
$ 0.1 0.05 0.0 0.0 20 1 1 0.0 1.0
$ 0.0 0.0 0.0 0.0 0.0 0 1 0 0
$-----1-----2-----3-----4-----5-----6-----7-----8
$ BOUNDARY PRESCRIBED MOTION RIGID
$-----1-----2-----3-----4-----5-----6-----7-----8
$ 4 3 2 1 1
*DEFINE CURVE
$-----1-----2-----3-----4-----5-----6-----7-----8
$ 1 0 0 1 1 0 0
$ 0.002 -1.26
$ .018 -21.42
$ .020 -21.68
$ .021 -21.68
*SET PART LIST
$-----1-----2-----3-----4-----5-----6-----7-----8
$ 1
*INTERFACE SPRINGBACK DYNA3D NOTHICKNESS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ 1
*END
$-----1-----2-----3-----4-----5-----6-----7-----8
*KEYWORD
$-----1-----2-----3-----4-----5-----6-----7-----8
$ DYN3D(936) DECK WAS WRITTEN BY: ETA/FEMB VERSION 26
$ DATE : Jan 24, 2002 at 10:35:52
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (1) TITLE CARD.
*TITLE
$-----1-----2-----3-----4-----5-----6-----7-----8
$ SPRINGBACK
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (2) CONTROL CARDS.
*CONTROL IMPLICIT STABILIZATION
$-----1-----2-----3-----4-----5-----6-----7-----8
$ 1
*CONTROL IMPLICIT GENERAL
$-----1-----2-----3-----4-----5-----6-----7-----8
$ 1 .005
*CONTROL TERMINATION
$-----1-----2-----3-----4-----5-----6-----7-----8
$ ENDTIM ENDCYC DTMIN ENDMIN ENDMAX
$ 0.020E+00 0 .000 .000
*CONTROL TIMESTEP
$-----1-----2-----3-----4-----5-----6-----7-----8
$ DTINIT SCPT ISDO TSLIMIT DIMS LCTM ERODE MSIST
$ .000 .900 0
*CONTROL HOURGLASS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ IHQ QH
$ 4 .100
*CONTROL BULK VISCOSITY
$-----1-----2-----3-----4-----5-----6-----7-----8
$ Q1 Q2
$ 1.500 .060
*CONTROL SHELL
$-----1-----2-----3-----4-----5-----6-----7-----8
$ WRPANG ITRIST IRNXX ISTUPD THEORY BWC MITER
$ 20.000 2 -1 1 2 2 1
*CONTROL CONTACT
$-----1-----2-----3-----4-----5-----6-----7-----8
$ SLSFAC RWPNAL ISLCHK SHLTHK PENOPT THKCHK ORLEN
$ .010 USRFAC NSBCS INTERM XPFEN
$ 0 0 0 10 0 4.000
*CONTROL ENERGY
$-----1-----2-----3-----4-----5-----6-----7-----8
$ HGEN RWEN SLTENT RYLEN
$ 1 2 1 1
*CONTROL DAMPING
$-----1-----2-----3-----4-----5-----6-----7-----8
$ NRCYCK DRTOL DRFCTR DRTERM TSSFDR IRELAL EDTLL IDRFLG
$ 250 .001 .995
*CONTROL OUTPUT
$-----1-----2-----3-----4-----5-----6-----7-----8
$ NFOPT NEECHO NREFUP IACCOP OPIFS IPNINT IKEDIT
$ 0 0 0 0 0 .000 0 100
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (3) DATABASE CONTROL CARDS - ASCII HISTORY FILE
$-----1-----2-----3-----4-----5-----6-----7-----8
$ SOPTION : BEAM BEAM_SET NODE NODE_SET
$ SHELL SHELL_SET SOLID SOLID_SET
$ TSHELL TSHELL_SET
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (4) DATABASE CONTROL CARDS FOR ASCII FILE
*DATABASE OPTION
$-----1-----2-----3-----4-----5-----6-----7-----8
$ DT
$-----1-----2-----3-----4-----5-----6-----7-----8
$ SOPTION : SPCFORC RMPORC NODOUT ELOUT GLSTAT
$ DEFORC MATSUM NCFORC RCFORC DEFORC
$ SPCFORC SPCFORC ABSTAT NODFORC BNDOUT
$ RBDOUT GCBOOUT SLEOUT MGSF SBTOUT
$ UNIFORM AVSFPLT MOVIE
*DATABASE WOODOT
$-----1-----2-----3-----4-----5-----6-----7-----8
$ 400E-04
*DATABASE ELOUT
$-----1-----2-----3-----4-----5-----6-----7-----8
$ 400E-04
*DATABASE GLSTAT
$-----1-----2-----3-----4-----5-----6-----7-----8
$ 400E-04
*DATABASE DEFORC
$-----1-----2-----3-----4-----5-----6-----7-----8
$ 400E-04
*DATABASE RBDOUT
$-----1-----2-----3-----4-----5-----6-----7-----8
$ 400E-04
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (5) DATABASE CONTROL CARDS FOR BINARY FILE
*DATABASE BINARY D3PLOT
$-----1-----2-----3-----4-----5-----6-----7-----8
$ DT/CYCL LCDD NOBEAM
$ 100E-02
*DATABASE BINARY D3THDT
$-----1-----2-----3-----4-----5-----6-----7-----8
$ DT/CYCL LCDD NOBEAM
$ 100E-02
*DATABASE BINARY OPTION
$-----1-----2-----3-----4-----5-----6-----7-----8
$ DT/CYCL LCDD NOBEAM
$-----1-----2-----3-----4-----5-----6-----7-----8
$ SOPTION : DIDRFL D3DUMP RUNRSP INTFOR
$-----1-----2-----3-----4-----5-----6-----7-----8
*DATABASE EXTENT BINARY
$-----1-----2-----3-----4-----5-----6-----7-----8
$ 0 0 3 1 1 1 1 1
$ 0 0 0 0 0 0 0 0
$-----1-----2-----3-----4-----5-----6-----7-----8

```

A2 Spring back Input Deck

```

$ (6) DEFINE PARTS CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
*PART
$ PART PID = 1 PART NAME :BLANK
$ PID SID MID EOSID HGID GRAV ADPOPT TMID
$ 1 1 3
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (7) MATERIAL CARDS
*MAT PIECEWISE LINEAR PLASTICITY
$ MATERIAL NAME:HRQ (Hot Rolled, Draw Quality Steel)
$ MID RO E PR SIGY ETAN EPPF TDEL
$ 3 7.830E-09 2.070E+05 3.000E-01 2.480E+02 0.000E+00 0.000E+00 0.000E+00
$ C P LCSS LCSS
$ .000E+00 .000E+00
$ EPS1 EPS2 EPS3 EPS4 EPS5 EPS6 EPS7 EPS8
$ 0.000E+00 5.000E-02 1.000E-01 1.500E-01 2.000E-01 2.500E-01 3.000E-01 3.500E-01
$ ES1 ES2 ES3 ES4 ES5 ES6 ES7 ES8
$ 2.480E+02 3.260E+02 3.730E+02 4.000E+02 4.150E+02 4.250E+02 4.350E+02 4.500E+02
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (7.1) SECTION CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
*SECTION SHELL
$ PROPERTY NAME:BLANK
$ SID ELFORM SHRP NIP PROPT QR/IRID ICOMP
$ 7 16 .100E+01 5.0 1.0 .0
$ T1 T2 T3 T4 NLGC
$ .200E+01 .200E+01 .200E+01 .200E+01 .0
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (8) NODAL POINT CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (14) HOURGLASS AND BULK PROPERTIES CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
*HOURGLASS
$ IHQ QH IBO Q1 Q2
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (15) DEFINE SET CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (16) BOUNDARY CONDITION CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (17) LOCAL COORDINATE SYSTEM
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (18) NODAL CONSTRAINT CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (22) DEFINE CONTACT SURFACE
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (24) NODAL RIGID BODY CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (23) DEFINE RIGID WALL
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (25) JOINT CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
*BOUNDARY_SPC_NODE
$ 53 0 1 1 1 0 0 0
$ 23 0 0 1 1 0 0 0
*SET_PART_LIST
$ 1
$-----1-----2-----3-----4-----5-----6-----7-----8
*INTERFACE_SPRINGBACK_DYN3D_NOTIHCNESS
$ 1
*INCLUDE
$ format$
$ END

```

A3 Crash Model Input Deck

```

*KEYWORD
$-----1-----2-----3-----4-----5-----6-----7-----8
$ DYN3D(936) DECK WAS WRITTEN BY: ETA/FEMB VERSION 26
$ DATE : Jan 28, 2002 at 14:02:54
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (1) TITLE CARD.
$-----1-----2-----3-----4-----5-----6-----7-----8
*TITLE
$ Crash Model, as rolled
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (2) CONTROL CARDS.
$-----1-----2-----3-----4-----5-----6-----7-----8
*CONTROL_TERMINATION
$ ENDTIM ENDCYC DTMIN ENDMEG ENDMAS
$ .015E+00 0 .000 .000 .000
*CONTROL_TIMESTEP
$ DTINIT SCPT ISDO TSLIMIT DTMS LCTM ERODE MS1ST
$ .000 .900 0
*CONTROL_HOURGLASS
$ IHQ QH
$ 1 .100
*CONTROL_BULK_VISCOSITY
$ Q2 Q1
$ 1.500 .060
*CONTROL_SHELL
$ WRPANG ITRIST IRNXX ISTDPT THEORY BWC MITER
$ 20.000 2 -1 0 2 2 1
*CONTROL_CONTACT
$ SLSFAC RMPNAL ISLCHK SHLTHK PENOPT THKCHG ORLEN
$ .100
$ USRSTR USRFAC NSBSC INTERM XPFNE
$ 0 0 10 0 4.000
*CONTROL_ENERGY
$ HGEN RWEN SLNTEN RYLEN
$ 1 2 1 1
*CONTROL_DAMPING
$ NRCYCK DRTOLE DRFCR DRTERM TSSPR IRELAL EDTLL IDRFLG
$ 250 .001 .995
*CONTROL_OUTPUT
$ NPOFT NEECHO NREPUF IACOP OPFIS IPNINT IKEDIT
$ 0 0 0 0 0 .000 0 100
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (3) DATABASE CONTROL CARDS - ASCII HISTORY FILE
$-----1-----2-----3-----4-----5-----6-----7-----8
*DATABASE_HISTORY_NODE
$ ID1 ID2 ID3 ID4 ID5 ID6 ID7 ID8
$ RAM CORNER1 CORNER2 CORNER3 CORNER4
$ 981 693 153 127 667
$ SHELL SHELL_SET NODE SET
$ SHELL SHELL_SET SOLID SOLID_SET
$ TSHELL TSHELL_SET
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (4) DATABASE CONTROL CARDS FOR ASCII FILE
$-----1-----2-----3-----4-----5-----6-----7-----8
*DATABASE_NODFOR
$ DT
$ .0001
*DATABASE_NODAL_FORCE_GROUP
$ 1
$ OPTION : SEPCORC RMPORC NODOUT ELOUT GLSTAT

```

```

$ DEFORC MATSUM NCFORC RCFORC DEFDEG
$ SPCFORC SWFORC ABSTAT NODFOR ENDOUT
$ BROOUT CROOUT SLOOUT MRGS SBTOUT
$ JNTOFOR AVSFLT MOVIE
*DATABASE_NODOUT
$ .200E-04
*DATABASE_GLSTAT
$ .200E-04
*DATABASE_DEFORC
$ .200E-04
*DATABASE_NODFOR
$ .200E-04
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (5) DATABASE CONTROL CARDS FOR BINARY FILE
$-----1-----2-----3-----4-----5-----6-----7-----8
*DATABASE_BINARY_D3PLOT
$ DT/CYCL LCDD NOBEAM
$ .500E-03
*DATABASE_BINARY_D3THDT
$ DT/CYCL LCDD NOBEAM
$ .500E-03
*DATABASE_BINARY_OPTION
$ DT/CYCL LCDD NOBEAM
$
$ OPTION : D3DRFL D3DUMP RUNRSP INTFOR
$-----1-----2-----3-----4-----5-----6-----7-----8
*DATABASE_EXTENT_BINARY
$ 0 0 3 1 1 1 1 1
$ 0 0 0 0 0 0 0 0
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (6) DEFINE PARTS CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
*PART
$ SHEADING
$ PART PID = 1 PART NAME :BLANK
$ PID SID MID EOSID HGID GRAV ADPOPT TMID
$ 1 1 3
$-----1-----2-----3-----4-----5-----6-----7-----8
*PART
$ SHEADING
$ PART PID = 2 PART NAME :BOTTOM
$ PID SID MID EOSID HGID GRAV ADPOPT TMID
$ 2 6 12
$-----1-----2-----3-----4-----5-----6-----7-----8
*PART
$ SHEADING
$ PART PID = 4 PART NAME :RAM
$ PID SID MID EOSID HGID GRAV ADPOPT TMID
$ 4 5 4
$-----1-----2-----3-----4-----5-----6-----7-----8
*PART
$ SHEADING
$ PART PID = 4 PART NAME :RAM
$ PID SID MID EOSID HGID GRAV ADPOPT TMID
$ 4 9 9
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (7) MATERIAL CARDS
*MAT PIECEWISE LINEAR PLASTICITY
$ MATERIAL NAME:HRQ (Ho
$ MID RO E PR SIGY ETAN EPPF TDEL
$ 3 7.830E-09 2.070E+05 3.000E-01 2.480E+02 0.000E+00 3.700E-01 0.000E+00
$ C P LCSS LCSS
$ .000E+00 .000E+00
$ EPS1 EPS2 EPS3 EPS4 EPS5 EPS6 EPS7 EPS8
$ 0.000E+00 5.000E-02 1.000E-01 1.500E-01 2.000E-01 2.500E-01 3.000E-01 3.500E-01
$ ES1 ES2 ES3 ES4 ES5 ES6 ES7 ES8
$ 2.480E+02 3.260E+02 3.730E+02 4.000E+02 4.150E+02 4.250E+02 4.350E+02 4.500E+02
*MAT_PIECEWISE_LINEAR_PLASTICITY
$ MID RO E PR SIGY ETAN EPPF TDEL
$ 4 7.830E-09 2.070E+05 2.800E-01 2.100E+02
$ C P LCSS LCSS
$ EPS1 EPS2 EPS3 EPS4 EPS5 EPS6 EPS7 EPS8
$ 0.000E+00 3.090E-02 4.090E-02 5.000E-02 1.510E-01 3.010E-01 7.010E-01 9.010E-01
$ ES1 ES2 ES3 ES4 ES5 ES6 ES7 ES8
$ 2.100E+02 3.000E+02 3.140E+02 3.250E+02 3.900E+02 4.380E+02 5.050E+02 5.270E+02
*MAT_RIGID
$ MATERIAL NAME:PUNCH
$ MID RO E PR N COUPLE M ALIAS
$ 12 7.830E-09 2.070E+05 2.800E-01 0.000E+00 0.000E+00 0.000E+00
$ CMO CON1 CON2
$ 1.0 7.0 7.0
$ SLCO or A1 A2 A3 V1 V2 V3
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (7.1) SECTION CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
*SECTION SHELL
$ PROPERTY NAME:BLANK
$ SID ELFORM SHRP NIP PROPT QR/IRID ICOMP
$ 7 16 .100E+01 5.0 1.0 .0
$ T1 T2 T3 T4 NLGC
$ 2.000E+00 2.000E+00 2.000E+00 2.000E+00
*SECTION_SHELL
$ PROPERTY NAME:RAM
$ SID ELFORM SHRP NIP PROPT QR/IRID ICOMP
$ 5 2 .100E+01 2.0 1.0 .0
$ T1 T2 T3 T4 NLGC
$ 6.000E+00 6.000E+00 6.000E+00 6.000E+00
*SECTION_SHELL
$ PROPERTY NAME:RAM
$ SID ELFORM SHRP NIP PROPT QR/IRID ICOMP
$ 5 2 .100E+01 2.0 1.0 .0
$ T1 T2 T3 T4 NLGC
$ 4.000E+00 4.000E+00 4.000E+00 4.000E+00
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (8) NODAL POINT CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
*NODE
$ NODE X Y Z TC RC
$ 1 .113365200E+02 .199141300E+02 .420567000E+01
$ 2 .140417200E+02 .199264900E+02 .125913400E+01
$ 3 .167468200E+02 .199388500E+02 .168741700E+01
$ 4 .194519200E+02 .199512300E+02 .463397200E+01
$ 5 .221571800E+02 .199636100E+02 .758042500E+01
$ 6 .248625000E+02 .199760000E+02 .105276600E+02
$ 7 .275656700E+02 .199885000E+02 .134752200E+02
$ 8 .302677800E+02 .200009300E+02 .164249400E+02
$ 9 .330318000E+02 .200119600E+02 .193224200E+02
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (9) SOLID ELEMENT CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
*ELEMENT_SOLID
$ EID PID N1 N2 N3 N4 N5 N6 N7 N8
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (10) BEAM ELEMENT CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
*ELEMENT_BEAM
$ EID PID N1 N2 N3
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (11) SHELL ELEMENT CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
*ELEMENT_SHELL
$ EID PID N1 N2 N3 N4
$ 101 2 127 154 155 128
$ 102 2 128 155 156 129
$ 103 2 129 156 157 130
$ 104 2 130 157 158 131
$ 105 2 131 158 159 132
$ 106 2 132 159 160 133
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (12) SPRING OR DAMPER ELEMENT CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
*ELEMENT_DISCRETE
$ EID PID N1 N2 VID S PP
$ 621 9 693 697 0 .1000000E+01 0 .0000000E+00

```

```

$ 622 9 667 694 0 .1000000E+01 0 .0000000E+00
$ 623 9 127 695 0 .1000000E+01 0 .0000000E+00
$ 624 9 153 696 0 .1000000E+01 0 .0000000E+00
*ELEMENT_MASS
$ EID NID MASS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (14) HOURGLASS AND BULK PROPERTIES CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
$*HOURGLASS
$ IHO QH IBQ Q1 Q2
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (15) DEFINE SET CARDS
*INITIAL_VELOCITY
$-----1-----2-----3-----4-----5-----6-----7-----8
$ 1
$ 0 0 4705.6 0 0 0
*SET_NODE_LIST
$ SID DA1 DA2 DA3 DA4
$ 1
$ NID1 NID2 NID3 NID4 NID5 NID6 NID7 NID8
698 699 700 701 702 703 704 705
706 707 708 709 710 711 712 713
714 715 716 717 718 719 720 721
722 723 724 725 726 727 728 729
730 731 732 733 734 735 736 737
738 739 740 741 742 743 744 745
746 747 748 749 750 751 752 753
754 755 756 757 758 759 760 761
762 763 764 765 766 767 768 769
770 771 772 773 774 775 776 777
778 779 780 781 782 783 784 785
786 787 788 789 790 791 792 793
794 795 796 797 798 799 800 801
802 803 804 805 806 807 808 809
810 811 812 813 814 815 816 817
818 819 820 821 822 823 824 825
826 827 828 829 830 831 832 833
834 835 836 837 838 839 840 841
842 843 844 845 846 847 848 849
850 851 852 853 854 855 856 857
858 859 860 861 862 863 864 865
866 867 868 869 870 871 872 873
874 875 876 877 878 879 880 881
882 883 884 885 886 887 888 889
890 891 892 893 894 895 896 897
898 899 900 901 902 903 904 905
906 907 908 909 910 911 912 913
914 915 916 917 918 919 920 921
922 923 924 925 926 927 928 929
930 931 932 933 934 935 936 937
938 939 940 941 942 943 944 945
946 947 948 949 950 951 952 953
954 955 956 957 958 959 960 961
962 963 964 965 966 967 968 969
970 971 972 973 974 975 976 977
978 979 980 981 982 983 984 985
986 987 988 989 990 991 992 993
994 995 996 997 998 999 1000 1001
1002 1003 1004 1005 1006 1007 1008 1009
1010 1011 1012 1013 1014 1015 1016 1017
1018 1019 1020 1021 1022 1023 1024 1025
1026 1027 1028 1029 1030 1031 1032 1033
1034 1035 1036 1037 1038 1039 1040 1041
1042 1043 1044 1045 1046 1047 1048 1049
1050 1051 1052 1053 1054 1055 1056 1057
1058 1059 1060 1061 1062 1063 1064 1065
1066 1067 1068 1069 1070 1071 1072 1073
1074 1075 1076 1077 1078 1079 1080 1081
1082 1083 1084 1085 1086 1087 1088 1089
1090 1091 1092 1093 1094 1095 1096 1097
1098 1099 1100 1101 1102 1103 1104 1105
1106 1107 1108 1109 1110 1111 1112 1113
1114 1115 1116 1117 1118 1119 1120 1121
1122 1123 1124 1125 1126 1127 1128 1129
1130 1131 1132 1133 1134 1135 1136 1137
1138 1139 1140 1141 1142 1143 1144 1145
1146 1147 1148 1149 1150 1151 1152 1153
1154 1155 1156 1157 1158 1159 1160 1161
1162 1163 1164 1165 1166 1167 1168 1169
1170 1171 1172 1173 1174 1175 1176 1177
1178 1179 1180 1181 1182 1183 1184 1185
1186 1187 1188 1189 1190 1191 1192 1193
1194 1195 1196 1197 1198 1199 1200 1201
1202 1203 1204 1205 1206 1207 1208 1209
1210 1211 1212 1213 1214 1215 1216 1217
1218 1219 1220 1221 1222 1223 1224 1225
1226 1227 1228 1229 1230 1231 1232 1233
1234 1235 1236 1237 1238 1239 1240 1241
1242 1243 1244 1245 1246 1247 1248 1249
1250 1251 1252 1253 1254 1255 1256 1257
1258 1259 1260 1261 1262 1263 1264
*SET_SHELL_LIST
$ SID NUM DA1 DA2 DA3 DA4
$ 12 40
$ EID5 EID2 EID3 EID4 EID5 EID6 EID7 EID8
7 8 9 10 11 12 13 14
27 28 29 30 31 32 33 34
47 48 49 50 51 52 53 54
67 68 69 70 71 72 73 74
87 88 89 90 91 92 93 94
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (16) BOUNDARY CONDITION CARDS
*BOUNDARY_SPC_NODE
$ NID/NSID CID DOFX DOFY DOFZ DOFRX DOFRY DOFRZ
698 0 1 1 0 0 0 0
751 0 1 1 0 0 0 0
1238 0 1 0 0 0 0 0
1264 0 1 1 0 0 0 0
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (17) LOCAL COORDINATE SYSTEM
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (18) NODAL CONSTRAINT CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (22) DEFINE CONTACT SURFACE
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (23) DEFINE RIGID WALL
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (24) NODAL RIGID BODY CARDS
$-----1-----2-----3-----4-----5-----6-----7-----8
$ (25) JOINT CARDS
*SECTION_DISCRETE
$ SID DRO KD VO CL FD
$ 9 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00
$ CDL TDL
0.000E+00 0.000E+00
$-----1-----2-----3-----4-----5-----6-----7-----8
*MAT_SPRING_ELASTIC
$ MAT MID K
9 2.000E+02
*SET_PART_LIST
$ 66
2 4
$-----1-----2-----3-----4-----5-----6-----7-----8
*CONTACT_AUTOMATIC_SURFACE_TO_SURFACE
$ 66 2 1 1
0.1 0.05 0.0 0.0 60 1 0.0 0.0

```

*INCLUDE
relstrs
*END

-forming analysis Dyna deck
-springback Dyna deck
-crash Dyna deck